

BUH515

HIGH VOLTAGE FAST-SWITCHING NPN POWER TRANSISTOR

- HIGH VOLTAGE CAPABILITY
- U.L. RECOGNISED ISOWATT218 PACKAGE (U.L. FILE # E81734 (N)).

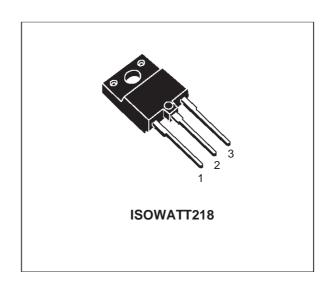
APPLICATIONS:

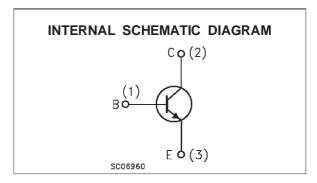
- HORIZONTAL DEFLECTION FOR COLOUR TV AND MONITORS
- SWITCH MODE POWER SUPPLIES



The BUH515 is manufactured using Multiepitaxial Mesa technology for cost-effective high performance and uses a Hollow Emitter structure to enhance switching speeds.

The BUH series is designed for use in horizontal deflection circuits in televisions and monitors.





ABSOLUTE MAXIMUM RATINGS

Symbol	Parameter	Value	Unit
V _{CBO}	Collector-Base Voltage (I _E = 0)	1500	V
V _{CEO}	Collector-Emitter Voltage (I _B = 0)	700	V
V _{EBO}	Emitter-Base Voltage (I _C = 0)	10	V
Ic	Collector Current	8	Α
I _{CM}	Collector Peak Current (t _p < 5 ms)	12	Α
I _B	Base Current	5	Α
I _{BM}	Base Peak Current (t _p < 5 ms)	8	Α
P _{tot}	Total Dissipation at T _c = 25 °C	50	W
T _{stg}	Storage Temperature	-65 to 150	°C
Tj	Max. Operating Junction Temperature	150	°C

November 1999 1/7

BUH515

THERMAL DATA

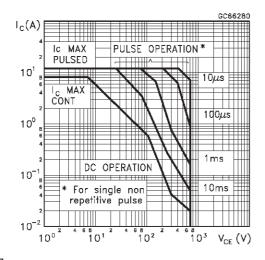
R _{thj-case}	Thermal Resistance Junction-case	Max	2.5	°C/W
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ELECTRICAL CHARACTERISTICS (T_{case} = 25 °C unless otherwise specified)

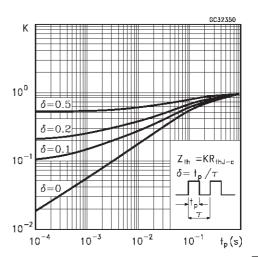
Symbol	Parameter	Test Conditions	Min.	Тур.	Max.	Unit
Ices	Collector Cut-off Current (V _{BE} = 0)	V _{CE} = 1500 V V _{CE} = 1500 V T _j = 125 °C			0.2 2	mA mA
I _{EBO}	Emitter Cut-off Current (I _C = 0)	V _{EB} = 5 V			100	μΑ
V _{CEO(sus)*}	Collector-Emitter Sustaining Voltage (I _B = 0)	I _C = 100 mA	700			\ \
V _{EBO}	Emitter-Base Voltage (Ic = 0)	I _E = 10 mA	10			V
V _{CE(sat)} *	Collector-Emitter Saturation Voltage	I _C = 5 A I _B = 1.25 A			1.5	٧
V _{BE(sat)} *	Base-Emitter Saturation Voltage	I _C = 5 A I _B = 1.25 A			1.3	V
h _{FE} *	DC Current Gain	$I_{C} = 5 \text{ A}$ $V_{CE} = 5 \text{ V}$ $I_{C} = 5 \text{ A}$ $V_{CE} = 5 \text{ V}$ $T_{j} = 100 ^{\circ}\text{C}$	6 4		12	
t _s	RESISTIVE LOAD Storage Time Fall Time	$V_{CC} = 400 \text{ V}$ $I_{C} = 5 \text{ A}$ $I_{B1} = 1.25 \text{ A}$ $I_{B2} = 2.5 \text{ A}$		2.7 190	3.9 280	μs ns
t _s	INDUCTIVE LOAD Storage Time Fall Time			2.3 350		μs ns
t _s	INDUCTIVE LOAD Storage Time Fall Time	$\begin{aligned} &I_{C} = 5A & f = 31250 \text{ Hz} \\ &I_{B1} = 1.25 \text{ A} &I_{B2} = -1.5 \text{ A} \\ &V_{\text{ceflyback}} = 1200 \text{ sin} \bigg(\frac{\pi}{5} 10^6 \bigg) t & V \end{aligned}$		2.3 200		μs ns

^{*} Pulsed: Pulse duration = 300 μs, duty cycle 1.5 %

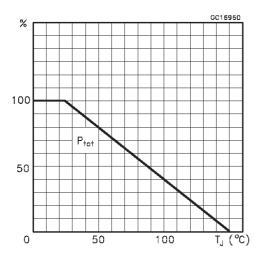
Safe Operating Area



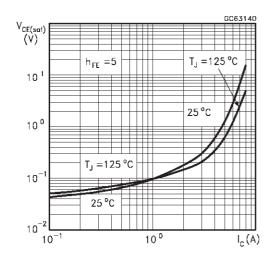
Thermal Impedance



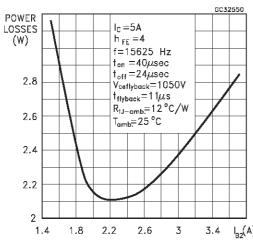
Derating Curve



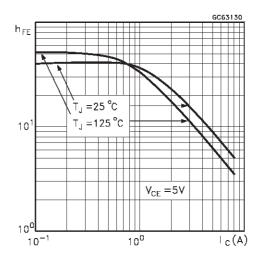
Collector Emitter Saturation Voltage



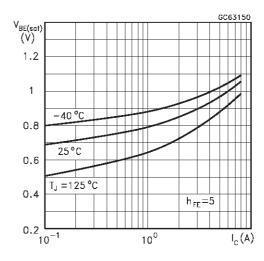
Power Losses at 16 KHz



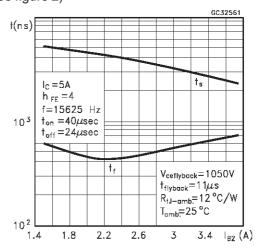
DC Current Gain



Base Emitter Saturation Voltage

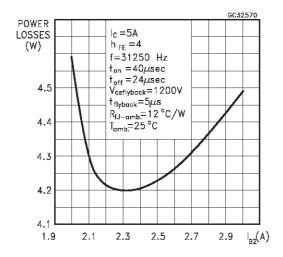


Switching Time Inductive Load at 16KHz (see figure 2)

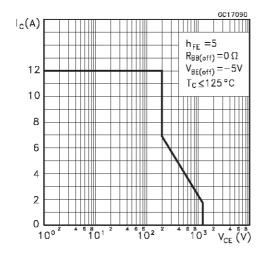


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Power Losses at 32 KHz



Reverse Biased SOA

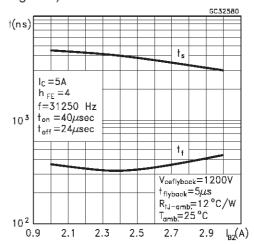


BASE DRIVE INFORMATION

In order to saturate the power switch and reduce conduction losses, adequate direct base current I_{B1} has to be provided for the lowest gain h_{FE} at 100 $^{\circ}$ C (line scan phase). On the other hand, negative base current I_{B2} must be provided to turn off the power transistor (retrace phase).

Most of the dissipation, in the deflection application, occurs at switch-off. Therefore it is essential to determine the value of I_{B2} which minimizes power losses, fall time t_f and, consequently, T_j . A new set of curves have been defined to give total power losses, t_s and t_f as a function of I_{B2} at both 16 KHz and 32 KHz scanning frequencies for choosing the optimum negative drive. The test circuit is illustrated in

Switching Time Inductive Load at 32 KHz (see figure 2)



Switching Time Resistive Load

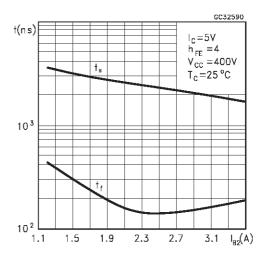


figure 1.

Inductance L_1 serves to control the slope of the negative base current $l_{\rm B2}$ to recombine the excess carrier in the collector when base current is still present, this would avoid any tailing phenomenon in the collector current.

The values of L and C are calculated from the following equations:

$$\frac{1}{2}L\left(I_{C}\right)^{2} = \frac{1}{2}C\left(V_{CEfly}\right)^{2} \qquad \omega = 2\pi f = \frac{1}{\sqrt{LC}}$$

Where I_C= operating collector current, V_{CEfly}= flyback voltage, f= frequency of oscillation during retrace.

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Figure 1: Inductive Load Switching Test Circuits.

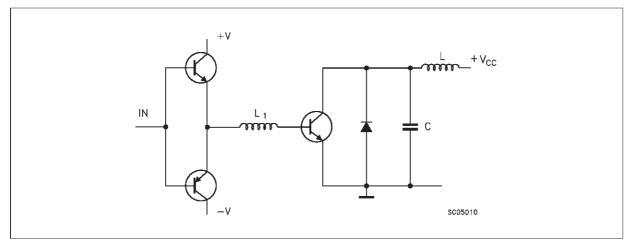
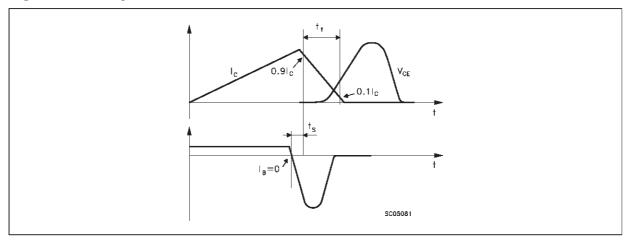
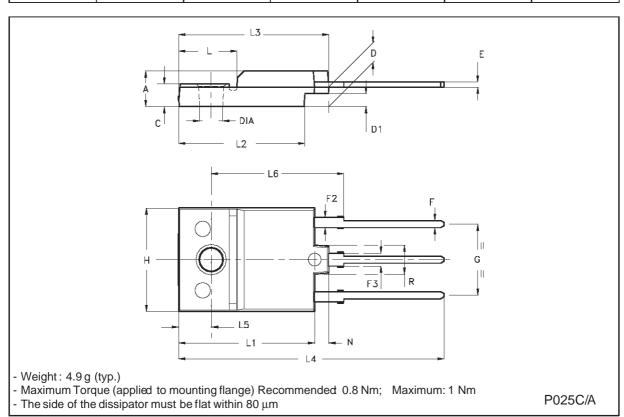


Figure 2: Switching Waveforms in a Deflection Circuit



ISOWATT218 MECHANICAL DATA

DIM.	mm		inch			
DIIVI.	MIN.	TYP.	MAX.	MIN.	TYP.	MAX.
А	5.35		5.65	0.211		0.222
С	3.30		3.80	0.130		0.150
D	2.90		3.10	0.114		0.122
D1	1.88		2.08	0.074		0.082
Е	0.75		0.95	0.030		0.037
F	1.05		1.25	0.041		0.049
F2	1.50		1.70	0.059		0.067
F3	1.90		2.10	0.075		0.083
G	10.80		11.20	0.425		0.441
Н	15.80		16.20	0.622		0.638
L		9			0.354	
L1	20.80		21.20	0.819		0.835
L2	19.10		19.90	0.752		0.783
L3	22.80		23.60	0.898		0.929
L4	40.50		42.50	1.594		1.673
L5	4.85		5.25	0.191		0.207
L6	20.25		20.75	0.797		0.817
N	2.1		2.3	0.083		0.091
R		4.6			0.181	
DIA	3.5		3.7	0.138		0.146



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